

Protective and Switching Devices Allocation According to Total Cost Minimization by Genetic Algorithm in Distribution Systems

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Abstract—Protective and switching devices play an important role in system reliability. The placement of these devices affects the effects of them. In this paper, novel method is proposed to allocate the protective and switching devices in distribution systems. In the proposed method, energy not supplied (ENS) is selected to define a proper objective function to find the optimal solution. One of the most effective advantages of the proposed method is the cost-benefit analysis in solve the optimization problem. The practical distribution network is selected to apply the method. The obtained results illustrate the effectiveness of the method.

Index Terms-- optimum protection, distribution networks, protective devices, switching devices, total cost, energy not supplied (ENS)

I. INTRODUCTION

THE fundamental purpose of the electric utilities is to service their customers with a reliable and appropriate cost power supply. In the recent studies, the most common indices used about the power quality and reliability of the distribution systems are customer oriented indices. These customer oriented indices are system average interruption frequency index (SAIFI), system average interruption duration index (SAIDI), average system interruption frequency index (ASIFI), average system interruption duration index (ASIDI), customer average interruption duration index (CAIDI), average system availability index (ASAI) and energy not supplied (ENS). These indices have been detailed in several relevant papers with the reliability of the distribution systems [1, 2].

Optimized and safe designing of distribution systems concludes the protective and switching devices in strategic places of the distribution networks to improve the reliability and power quality indices. Several papers are found in literature dealt with the optimized placement of protective and switching devices. References [3-7] survey separately the optimal switch allocation for network energy restoration. Other references have analyzed the optimized allocation of the

protective devices in distribution systems [1, 8-10]. Also several papers proposed different methods to optimally place both switches and protective devices [11-14].

In the model proposed in [3], the objective function includes outage, capital cost and maintenance to find the optimal placement of the switches. In other reference [4], the proposed method has dealt with the comparison between cost of the non-supplied energy and cost of the sectionalizing switches. The algorithm used to solve the optimization problem is genetic algorithm. [8]. Binary linear programming model is used for the placement of protection devices, fault locators and other sensors in the distribution networks [1, 9]. In References [11, 13], the problem of the optimized switches and protective devices is modeled through non-linear programming (MINLP) with real and binary variables. The reactive taboo search algorithm (RTS) is used to solve the optimized problem. Ref [14] has presented a multi objective optimization methodology to optimally place of the switches and protective devices to improve the system reliability indices. The multi objective ant colony optimization (MACO) has been applied to solve the problem. The proposed placement of switches and protective devices leads to minimize the total cost while simultaneously minimize two distribution network reliability indices including SAIFI and SAIDI.

This article tries to determine the location of protective and switching equipment including recloser, sectionalizer, fuse and isolator. In this method a general program has been designed firstly to receive data of network with the several formats from database then energy not supplied index will be calculated. The cost of energy not supplied (CENS) and the cost of install, repair and maintenance of devices is considered as an objective function. New method is introduced to calculate the interrupted loads and restoration energy. The introduced method is based on the analytical methods. One advantage of the proposed method is the ability of calculating different indices. Genetic Algorithm (GA) is selected to solve the optimization problem. The proposed method is applying to a real distribution system. The results illustrate the effectiveness of the proposed method.

II. OBJECTIVE FUNCTION

In this paper, a new objective function is defined to

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optimize the protective and switching devices allocation. The introduced objective function includes total cost of the distribution system. The total cost of each distribution system is the cost of the energy not supplied and the devices cost.

In Eq.1 the proposed objective function is shown. The cost of energy not supplied is a variable cost, while the devices cost is a fixed cost. Therefore, the variable cost would be added to fixed cost by a coefficient. This coefficient concludes several parameters such as useful lifetime of devices, load growth and the interest rate. In equations (1-3), the definition of the objective function is explained. In these equations, TC, FC, r, t, and p are the total cost of the distribution system, the cost of the device install and maintenance, the interest rate, useful time of devices and the load growth, respectively.

$$TC = FC + K \times CENS \quad (1)$$

$$q = \frac{1 + r\%}{1 + p\%} \quad (2)$$

$$K = \frac{q^t - 1}{q - 1} \quad (3)$$

Equations used to calculate the CENS and FC are shown in (4-10). The method of calculating the reliability indices introduced in [16] is used to calculate the CENS. Five main functions calculate the load interrupted and restoration energy in the distribution system.

$$F_1(X) = \sum_{i=1}^{mb} \lambda_{mj} \cdot \left(\sum_{j=i}^{mb} X_{mj} + \sum_{k=1}^{j-1, j+1} X_{mk} \cdot A(k+1, i) \right) + \sum_{s=1}^{f(b(i))} \sum_{p=1}^{n(s)} X(s, p) + \sum_{q=1}^{f(b(i))} \sum_{r=1}^{n(q)} X(q, r) \cdot A(fdmb(q), i) \quad (4)$$

$$F_2(X) = \sum_{s=1}^{f(b(i))} \sum_{p=1}^{n(s)} \lambda(s, p) \cdot \left(\sum_{j=1}^{mb} X_{mj} \cdot A(1, p) + \sum_{t=1}^{f(b(fdmb(s)))} \sum_{p=1}^{n(t)} X(t, p) \cdot A(1, w) \right) + \sum_{v=1}^{b(b(fdmb(s)))} \sum_{y=1}^{n(y)} X(v, y) \cdot A(fdmb(s), fumb(s)) \cdot A(1, w) + \sum_{l=1}^{fumb(s)-1} X_{ml} \cdot A(l, p) \cdot A(l, fdmb(s)) \quad (5)$$

Factor (1) and (2) are corresponded to interruption loads while fault occurs in network. Also factor (3), (4) and (5) calculate the restoration energy according to the ability of the switching devices. All variables used in these equations are explained in appendix.

To simplify the calculation of the introduced functions, two auxiliary functions are defined. The value of these auxiliary functions determines there is switching or protective device between two sections. The mathematical expressions of these functions are explained in Eqs (9) and (10).

The calculating the ENS and CENS are possible by using the introduced function. Because these functions are general, calculating the other reliability indices is easy. In Eqs. (11) and (12), the needed relations to calculate the ENS and CENS are

explained.

$$F_3(X) = \sum_{i=1}^{mb} Y_{si} \cdot \left(\sum_{j=1}^{mb} \lambda_{mj} \cdot A(i, j) \cdot \sum_{k=1}^{j-1} X_{mk} \cdot A(k+1, i-1) \cdot B(k+1, i-1) \right) + \sum_{n=f(b(1))-f(b(i))+1}^{f(b(1))} \sum_{p=1}^{n(n)} \lambda(n, p) \cdot A(1, ts(n)) \cdot A(i, fumb(n)) + \sum_{q=1}^{i-1} X_q \cdot B(q+1, i-1) \cdot A(1, i-1) \quad (6)$$

$$F_4(X) = \sum_{i=1}^{mb} Y_{si} \cdot \left(\sum_{j=1}^{mb} \lambda_{mj} \cdot A(i, j) \cdot \sum_{k=1}^{b(b(i))} \sum_{l=1}^{n(k)} X(k, l) \cdot A(fdmb, i-1) \cdot B(fdmb(k), i-1) \right) + \sum_{n=f(b(1))-f(b(i))+1}^{f(b(1))} \sum_{p=1}^{n(n)} \lambda(n, p) \cdot A(1, ts(n)) \cdot A(1, fumb(n)) + \sum_{q=1}^{b(b(i))} \sum_{r=1}^{n(q)} X(q, r) \cdot B(fdmb(q), i-1) \cdot A(fdmb(q), i-1) \quad (7)$$

$$F_5(X) = \sum_{i=1}^{mb} Y_{si} \cdot \left(\left\{ \sum_{k=1}^{b(b(i))} \sum_{l=1}^{n(k)} \lambda(k, l) \cdot A(1, l) \cdot B(1, fumb(k)) + \sum_{w=1}^{i-1} \lambda_w \cdot B(1, w) \right\} \cdot \text{Min} \left(\left\{ \sum_{n=f(b(1))-f(b(i))+1}^{f(b(i))} \sum_{p=1}^{n(n)} X(n, p) + \sum_{v=i+1}^{mb} X_{mv} \right\}, \sum_{r \in \beta} M_r \cdot P_r \right) \right) \quad (8)$$

$$A(i, j) = \begin{cases} 1 & \text{if exist no protective object in position } i \text{ to } j \\ 0 & \text{otherwise} \end{cases} \quad (9)$$

$$B(i, j) = \begin{cases} 1 & \text{if exist no switching object in position } i \text{ to } j \\ 0 & \text{otherwise} \end{cases} \quad (10)$$

$$ENS = \left[\sum_{i=1,2} F_i(L) \cdot T_1 - \sum_{i=3,4,5} F_i(L) \cdot T_2 \right] \quad (11)$$

$$CENS = \left[\sum_{i=1,2} F_i(L) \cdot CE - \sum_{i=3,4,5} F_i(L) \cdot (CE - CR) \right] \quad (12)$$

The main difference between Eqs. (11) and (12) is the cost coefficients and time coefficients. In Eq. (11), T_1 and T_2 are needed time to repair the interruption and restoration process by switching devices. The variables CE and CR are cost of the interruption and restoration while a fault occurs in system.

III. OBJECTIVE FUNCTION OPTIMIZATION

To find the optimum solution, the proposed objective function should be optimized. According to its non linear characteristic and complexity, optimization is not possible by using the conventional methods. Genetic algorithm is used to solve the optimization problem.

In Fig. 1, the flowchart of optimization by genetic algorithm is shown.

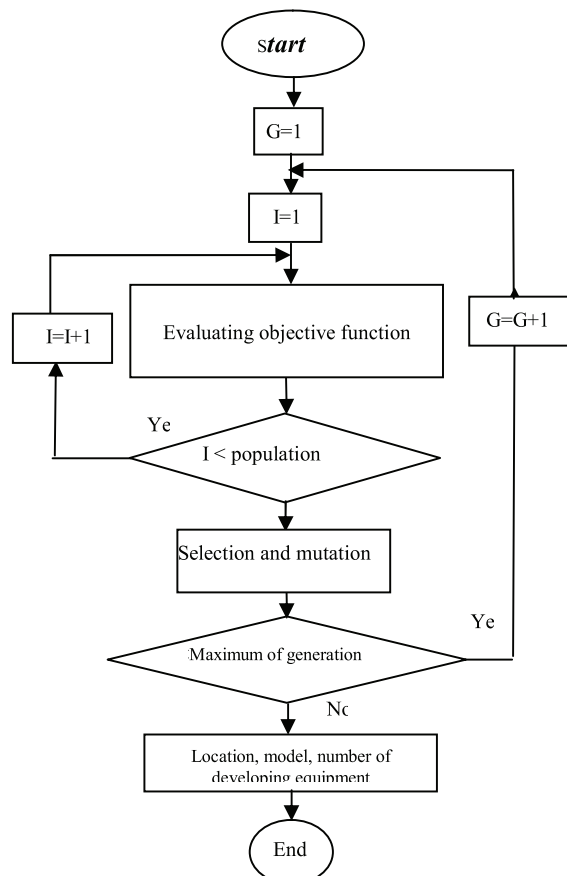


Figure 1: The flow-chart of the objective function optimization

IV. TEST RESULTS

To apply the method, a realistic distribution feeder is selected. The selected feeder is located in west of Tehran city. This feeder has 183 sections and works at 20 kV. The single line diagram of the feeder is shown in Fig.2. The information about the placement of the available devices in the system is demonstrated in Table I. The coefficients needed to solve the optimization are explained in Tables II and III. The value of coefficients have been extracted from references [11,12].

TABLE I
CURRENT CONDITION OF THE FEEDER

Device Type	NUMBER	Cost(\$)
RECLOSER	0	0
FUSE	7	3500
ISOLATOR	11	16500
BREAKER	4	13000
Fixed Cost		33000
CENS		35430
Total Cost		57342

TABLE II
DEVICES COST

Device Type	Cost (\$)
Recloser	1400
Sectionalizer	6500
Isolator	1500
Fuse	500

TABLE III
SUGGESTED PLACEMENT TO ALLOCATE DEVICES

Suggested Placement of Protective Devices	Suggested Placement of Switching Devices
11,16,28,48,58,105,119,121,128,131,152,160,178,157,159,36,45,54,56,124,127,129	117,103,54,51,45,36,14,2,179,15,6,159,143,137,183

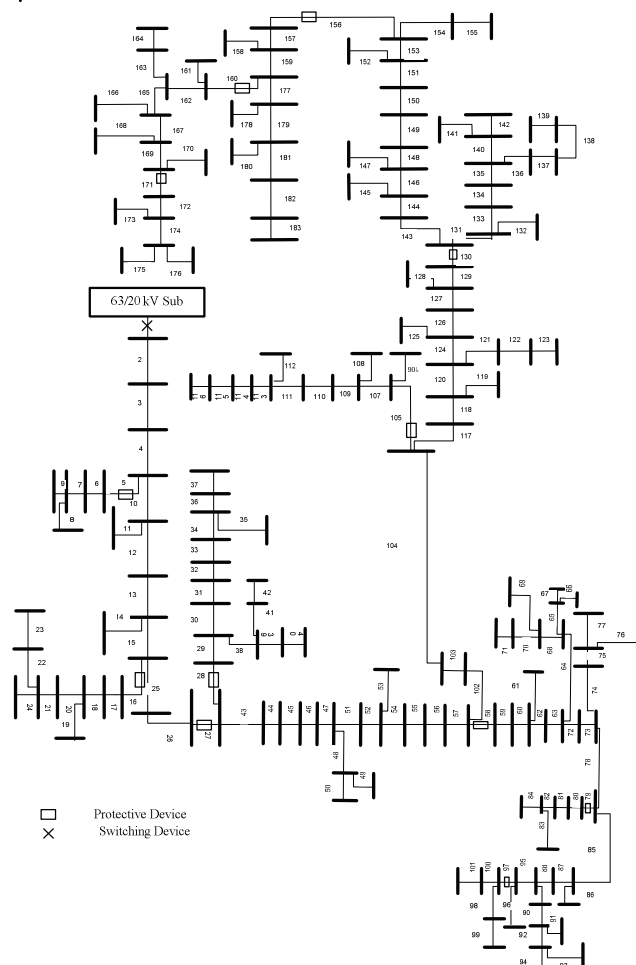


Figure 2: The single line diagram of the studied feeder

TABLE V
COMPONENT DATA FOR ANALYZED FEEDER

Permanent Failure rate (F/year)	Length (m)	Installed load (kVA)	Number of branch	Permanent Failure rate (F/year)	Length (m)	Installed load (kVA)	Number of branch	Permanent Failure rate (F/year)	Length (m)	Installed load (kVA)	Number of branch	Permanent Failure rate (F/year)	Length (m)	Installed load (kVA)	Number of branch	Permanent Failure rate (F/year)	Length (m)	Installed load (kVA)	Number of branch
0.04	200	0	149	0.048	240	150	200	0.048	240	151	0	0.066	330	152	200	0.32	1600	153	0
0.05	250	0	153	0.03	150	154	200	0.05	250	155	315	0.05	250	156	100	0.012	60	157	0
0.036	180	0	157	0.03	150	158	50	0.036	180	159	0	0.08	400	160	0	0.1	500	161	100
0.014	70	0	165	0.014	70	166	0	0.014	70	167	0	0.09	450	168	50	0.09	450	169	0
0.042	210	0	173	0.042	210	174	200	0.042	210	175	50	0.06	300	176	0	0.04	200	177	0
0.052	260	0	174	0.052	260	175	50	0.052	260	176	0	0.06	300	177	0	0.06	300	178	100
0.06	300	0	175	0.06	300	176	0	0.06	300	177	0	0.06	300	178	100	0.05	250	179	0
0.003	15	100	112	0.028	140	113	100	0.028	140	114	200	0.046	230	115	0	0.002	10	116	0
0.01	50	0	116	0.024	120	117	100	0.024	120	118	0	0.002	10	119	25	0.07	350	120	0
0.003	370	0	120	0.014	70	121	0	0.014	70	122	0	0.008	40	123	0	0.006	30	124	0
0.006	30	0	123	0.006	30	124	0	0.006	30	125	200	0.03	150	126	100	0.062	310	127	0
0.04	200	0	127	0.04	200	128	100	0.04	200	129	500	0.03	150	130	0	0.024	120	131	0
0.006	30	0	130	0.006	30	131	0	0.006	30	132	100	0.002	10	133	100	0.08	400	134	160
0.084	420	160	134	0.084	420	135	0	0.084	420	136	0	0.03	150	137	0	0.03	150	138	200
0.024	120	0	138	0.024	120	139	200	0.024	120	140	0	0.044	220	141	100	0.002	10	142	0
0.008	40	0	142	0.008	40	143	0	0.008	40	144	0	0.024	120	145	200	0.008	40	146	0
0.012	60	0	146	0.012	60	147	50	0.012	60	148	50	0.003	15	149	0	0.003	15	150	0
0.004	20	0	75	0.05	250	76	200	0.05	250	77	160	0.048	240	78	0	0.024	120	79	100
0.032	160	315	80	0.032	160	81	200	0.032	160	82	0	0.076	380	83	100	0.003	15	84	25
0.004	25	70	84	0.06	300	85	200	0.06	300	86	0	0.028	140	87	200	0.012	60	88	100
0.066	330	0	88	0.066	330	89	0	0.066	330	90	250	0.11	550	91	0	0.001	5	92	200
0.114	570	200	92	0.114	570	93	0	0.114	570	94	0	0.006	30	95	50	0.07	350	96	0
0.02	1000	0	93	0.2	1000	94	0	0.2	1000	95	50	0.07	350	96	0	0.07	350	97	50
0.006	30	0	94	0.006	30	95	50	0.006	30	96	0	0.07	350	97	50	0.07	350	98	315
0.01	500	0	95	0.01	500	96	0	0.01	500	97	50	0.02	100	98	315	0.06	300	99	315
0.012	60	0	102	0.012	60	103	0	0.012	60	104	0	0.01	50	105	0	0.01	50	106	100
0.036	180	0	104	0.036	180	105	0	0.036	180	106	100	0.036	180	107	0	0.036	180	108	0
0.024	120	0	108	0.024	120	109	250	0.024	120	110	250	0.04	200	111	0	0.04	200	112	100
0.042	210	0	74	0.042	210	75	0	0.042	210	76	200	0.05	250	77	0	0.05	250	78	0
0.01	50	0	39	0.01	50	40	0	0.01	50	41	0	0.07	350	42	0	0.07	350	43	425
0.072	360	0	41	0.072	360	42	0	0.072	360	43	425	0.028	140	44	0	0.002	10	45	0
0.02	100	0	42	0.02	100	43	425	0.02	100	44	0	0.002	10	45	0	0.008	40	46	0
0.008	40	0	46	0.008	40	47	0	0.008	40	48	0	0.126	630	49	50	0.002	10	50	200
0.12	600	0	50	0.12	600	51	200	0.12	600	52	0	0.026	130	53	200	0.003	15	54	500
0.002	10	0	51	0.002	10	52	0	0.002	10	53	200	0.003	15	54	500	0.02	100	55	250
0.012	60	0	55	0.012	60	56	200	0.012	60	57	0	0.038	190	58	250	0.07	350	59	0
0.09	450	0	56	0.09	450	57	0	0.09	450	58	250	0.07	350	59	0	0.036	180	60	0
0.038	190	0	57	0.038	190	58	250	0.038	190	59	0	0.036	180	60	0	0.036	180	61	500
0.07	350	0	58	0.07	350	59	0	0.07	350	60	0	0.036	180	61	500	0.07	350	62	100
0.01	50	0	62	0.01	50	63	0	0.01	50	64	0	0.032	160	65	100	0.03	150	66	0
0.032	160	0	63	0.032	160	64	0	0.032	160	65	100	0.03	150	66	0	0.03	150	67	100
0.07	350	0	64	0.07	350	65	100	0.07	350	66	0	0.003	15	67	100	0.036	180	68	200
0.003	15	0	66	0.003	15	67	100	0.003	15	68	200	0.036	180	69	100	0.084	420	70	200
0.036	180	0	67	0.036	180	68	200	0.036	180	69	100	0.084	420	70	200	0.048	240	71	160
0.024	120	0	71	0.024	120	72	500	0.024	120	73	0	0.014	70	74	100	0.06	300	75	0
0.042	210	0	72	0.042	210	73	0	0.042	210	74	100	0.06	300	75	0	0.06	300	76	200
0.014	70	0	73	0.014	70	74	100	0.014	70	75	0	0.003	15	76	200	0.05	250	77	160
0.004	20	0	75	0.004	20	76	200	0.004	20	77	160	0.048	240	78	0	0.024	120	79	100
0.048	240	0	76	0.048	240	77	160	0.048	240	78	0	0.024	120	79	100	0.048	240	80	315
0.024	120	0	78	0.024	120	79	100	0.024	120	80	315	0.032	160	81	200	0.024	120	82	0
0.076	380	0	82	0.076	380	83	100	0.076	380	84	25	0.014	70	85	200	0.06	300	86	0
0.003	15	0	83	0.003	15	84	25	0.003	15	85	200	0.06	300	86	0	0.028	140	87	200
0.014	70	0	84	0.014	70	85	200	0.014	70	86	0	0.028	140	87	200	0.012	60	88	100
0.06	300	0	85	0.06	300	86	0	0.06	300	87	200	0.012	60	88	100	0.066	330	89	0
0.028	140	0	86	0.028	140	87	200	0.028	140	88	100	0.066	330	89	0	0.028	140	90	250
0.002	10	0	87	0.002	10	88	100	0.002	10	89	0	0.028	140	90	250	0.11	550	91	0
0.001	5	0	91	0.001	5	92	200	0.001	5	93	0	0.1000	1000	94	0	0.006	30	95	50
0.114	570	200	92	0.114	570	93	0	0.114	570	94	0	0.006	30	95	50	0.07	350	96	0
0.2	1000	0	93	0.2	1000	94	0	0.2	1000	95	50	0.07	350	96	0	0.07	350	97	50
0.006	30	0	94	0.006	30	95	50	0.006	30	96	0	0.07	350	97	50	0.07	350	98	315
0.01	500	0	95	0.01	500	96	0	0.01	500	97	50	0.02	100	98	315	0.06	300	99	315
0.07	350	0	96	0.07	350	97	50	0.07	350	98	315	0.06	300	99	315	0.06	300	100	200
0.02	100	0	97	0.02	100	98	315	0.02	100	99	315	0.06	300	100	200	0.06	300	101	50
0.01	50	0	98	0.01	50	99	315	0.01	50	100	200	0.06	300	101	50	0.126	630	102	0
0.06	300	0	99	0.06	300	100	200	0.06	300	101	50	0.126	630	102	0	0.002	10	103	0
0.126	630	0	101	0.126	630	102	0	0.126	630	103	0	0.01	50	104	0	0.012	60	105	0
0.002	10	0	102	0.002	10	103	0	0.002	10	104	0	0.01	50	105	0	0.01	50	106	100
0.01	50	0	103	0.01	50	104	0	0.01	50	105	0	0.01	50	106	100	0.03	150	107	0
0.012	60	0	104	0.012	60	105	0	0.012	60	106	100	0.03	150	107	0	0.036	180	108	0
0.01	50	0	105	0.01	50	106	100	0.01	50	107	0	0.036	180	108	0	0.036	180	109	250
0.003	15	0	106	0.003	15	107	0	0.003	15	108	0	0.008	40	109	250	0.012	60	110	250
0.036	180	0	107	0.036	180	108	0	0.036	180	109	250	0.012	60	110	250	0.04	200	111	0
0.008	40	0	108	0.008	40	109	250	0.008	40	110	250	0.04	200	111	0	0.003	15	112	100
0.012	60	0	109	0.012	60	110	250	0.012	60	111	0	0.003	15	112	100	0.003	15	113	100

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